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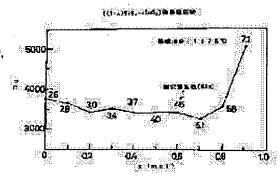
OZEKI HIROBUMI

(54) MICROWAVE DIELECTRIC PORCELAIN COMPOSITE, AND ITS MANUFACTURE

(57)Abstract:

PURPOSE: To provide a microwave dielectric porcelain composite of simple composition in which Qu, εr, and τf are all maintained within practical characteristic ranges, while indicating a high sintering density.

CONSTITUTION: A composite is expressed by a composition formula of (1-x)TiO2- xSnO2, where $0.8 \le x < 1.0$. Espacially, with x=0.9, and a baking temperature of 1375° C, then Qu=5040 (7.1GHz). εr=14.0, and τf=+1.2ppm/° C, which achieves excellent performance of the maximum Qu value and τf around 0, though εr is relatively small. This composite is manufactured by mixing titanium oxide (IV) powder with tin oxide (IV) powder, temporarily baking this mix to be temporarily baked powder, crushing the temporarily baked powder, moulding it in a specified form, and then baking it at 1275-1400° C.



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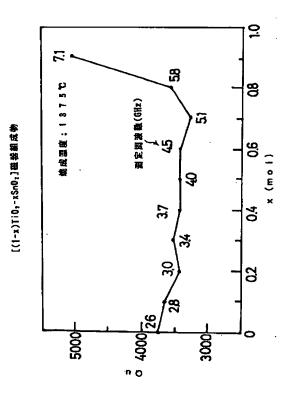
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(54) 【発明の名称】マイクロ波誘電体磁器組成物及びその製造方法

(57)【要約】

【目的】 Qu、 ϵ r及び τ rをいずれも実用的な特性 範囲に維持しつつ、高い焼結密度を示す、単純組成のマ イクロ波誘電体磁器組成物を提供する。

【構成】 本組成物は、組成式(1-x) TiO2-x SnO₂ 〔但し、0.8≤x<1.0〕で表される組成 からなる。特に x が 0.9で且つ焼成温度が 1375℃ では、Quが5040 (7.1GHz)、 $\epsilon_r = 14$. 0、 $\tau_{f} = +1$. 2ppm/ Cとなり、 ϵ_{r} はやや小さ いものの、Quは最大値を示し、τ、も0付近となり、 極めて優れた性能を示す。この組成物は、所定の組成に なるように酸化チタン(IV)粉末及び酸化錫(IV) 粉末を混合し、その後、仮焼し仮焼粉末を製造し、該仮 焼粉末を粉砕し、所定形状に成形し、次いで、1275 ~1400℃にて焼成して製造される。



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【特許請求の範囲】

【請求項1】 組成式 (1-x) TiO₂ -xSnO₂ [但し、0.8 \leq x \leq 1.0] で表される組成からなることを特徴とするマイクロ波誘電体磁器組成物。

【請求項2】 組成式 (1-x) TiO₂-xSnO₂ 〔但し、0.8≤x<1.0〕で示される組成になるように酸化チタン (IV) 粉末及び酸化錫 (IV) 粉末を混合し、その後、仮焼し仮焼粉末を製造し、該仮焼粉末を粉砕し、所定形状に成形し、次いで、1275~1400℃にて焼成することを特徴とするマイクロ波誘電体 10磁器組成物の製造方法。

【発明の詳細な説明】

[0001]

【産業上の利用分野】本発明は、マイクロ波誘電体磁器組成物に関し、更に詳しく言えば、無負荷Q(以下、単にQuという。)、比誘電率(以下、単に ϵ , という。)及び共振周波数の温度係数(以下、単に τ , という。)をいずれも実用的な特性範囲で維持しつつ、高い焼結密度を示すマイクロ波誘電体磁器組成物に関するものである。本発明は、マイクロ波領域において誘電体共 20振器、マイクロ波集積回路基板、各種マイクロ波回路のインピーダンス整合等に利用される。

[0002]

【従来の技術】一般にマイクロ波やミリ波等の髙周波領域に使用される誘電体共振器や誘電体基板には、髙い無負荷Q及び高い誘電率を有し、しかも共振周波数の絶対値が小さいものが望まれている。つまり、マイクロ波誘電体磁器組成物(以下、単に誘電体磁器組成物という。)は、使用周波数が髙周波となるに従って誘電損失が大きくなる傾向にあるので、マイクロ波領域でQuの30大きな誘電体磁器組成物が望まれている。また組成式(1-x)TiO2-xSnO2系誘電体磁器材料としては、xが0.5のものが知られている(「セラミックエ学ハンドブック」(発行:日本セラミックス協会、P.1885)。

[0003]

【発明が解決しようとする課題】しかし、上記 TiO_2 $-SnO_2$ 系誘電体磁器材料では、Q(7GHz)が4500、 ϵ 、が43と大きいものの、 τ fが+250 p pm/ Cと非常に大きく、0 付近の小さな値に調整することが困難であるという問題があった。

【0004】本発明は、上記問題点を解決するものであり、Qu、 ϵ ,及び τ ,をいずれも実用的な特性範囲に維持しつつ、高い焼結密度を示す、単純組成の誘電体磁器組成物及びその製造方法を提供することを目的とする。

[0005]

【課題を解決するための手段】本発明者らは、単純組成 約0.4Torr、凍結温度-20~-40 $\mathbb C$ 、乾燥温の誘電体磁器組成物において、Qu、 ϵ r及び τ rをい 度40~50 $\mathbb C$ 、真空乾燥時間約20時間)により造粒ずれも実用的な特性範囲に維持しつつ、高い焼結密度を 50 し、この造粒された原料を用いて1トン/c m^2 のプレ

示す組成について種々検討した結果、 TiO_2-SnO_2 系において所定の組成割合にすることにより、飛躍的にQuが大きくなり、且つ τ fが0近辺に調節可能な組成範囲を見出して、本発明を完成するに至ったのである。即ち、本第1発明の誘電体磁器組成物は、組成式 (1-x) TiO_2-xSnO_2 [但し、0.8 \le x<1.0]で表される組成からなることを特徴とする。 【0006】本第2発明の誘電体磁器組成物の製造方法は、組成式 (1-x) TiO_2-xSnO_2 [但し、0.8 \le x<1.0]で示される組成になるように酸化チタン (IV) 粉末及び酸化錫 (IV) 粉末を混合し、その後、仮焼、粉砕を行って所定形状に成形し、次いで、1275~1400℃にて焼成することを特徴とする。

【0007】組成式 (1-x) TiO₂ -xSnO₂ において、xの範囲を0. 8以上1. 0未満としたのは、xが0. 8未満の場合は τ , が大きな正の値をとり、Quが相対的に小さな値を示す(即ちxが0. 9の場合飛躍的に大きな値となる。)からである。逆にこれが1. 0の場合は1400℃においてもうまく緻密化しないからである。焼成温度を1275~1400℃の範囲としたのは、1275℃より低い温度ではうまく緻密化しない場合があり、逆に1400℃を越えると特性が徐々に劣化するからである。

【0008】特に、表1に示す実験結果によれば、焼成温度が1375℃及び1325℃の場合(xが0.9)では、Quが飛躍的に増大した。例えば、xが0.9で且つ焼成温度が1375℃では、Quが5040(7.1GHz)、 $\epsilon_r=14.0$ 、 $\tau_r=+1.2ppm/$ ℃となり、 ϵ_r はやや小さいものの、Qu は最大値を示し、 τ_r も0付近となり、極めて優れたバランス性能を示している。更に、焼成温度に関しては、1275~1400℃という広い温度範囲内にて焼成しても、各性能のバラツキが比較的少ないとともに優れた性能を示している。

[0009]

【実施例】以下、実施例により本発明を具体的に説明する。 TiO_2 粉末(純度;99.95%)、 SnO_2 粉末(純度;99.3%)を出発原料として、組成式(1-x) TiO_2-xSnO_2 のxが変化した組成になるように、所定量(全量として約500g)を秤量、混合した。その後、ミキサーで乾式による混合($20\sim30$ 分)及び一次粉砕を施した後、大気雰囲気中にて10500℃の温度で2時間仮焼した。次いで、この仮焼粉末に適量の有機バインダー(29g)と水($400\sim450g$)を加え、 $20mm\phiのアルミナボールで、<math>90rpm$ 、23時間粉砕した。その後、真空凍結乾燥(真空度約0.4<math>Torr、凍結温度 $-20\sim-40$ ℃、乾燥温度 $40\sim50$ ℃、真空乾燥時間約20時間)により造粒

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ス圧で $19mm\phi \times 11mmt$ (高さ)の円柱状に成形した。

【0010】次に、この成形体を大気中、500℃、3時間にて脱脂し、その後、 $1275\sim1400$ ℃の範囲の各温度で、4時間焼成し、最後に両端面を約16mm $\phi \times 8$ mm t (高さ)の円柱状に研磨して、誘電体試料(表 $1\sim3$ のNo、 $1-1\sim1-22$ 、 $2-1\sim2-2$ 2及び $3-1\sim3-22$)とした。尚、上記仮焼工程における昇温速度は200℃/h及び降温速度は-200℃/h、この脱脂工程における昇温速度は50℃/h、焼成工程における昇温速度は100℃/h及び降温速度は-100℃/hであった。

*誘電体円柱共振器法(TE_{011} MODE)により、Qu、 ϵ ,及び τ fを測定した。焼結密度はアルキメデス法により測定した。尚、共振周波数は2.6~7.1GHzである。また、 τ ,は23~80℃の温度領域で測定し、 τ ,=($f_{80}-f_{23}$)/($f_{23}\times\Delta T$)、 ΔT =80℃-23℃=57℃にて算出した。これらの結果を表1~3(焼成温度;1275~1400℃)及び図1~4(焼成温度;1375℃)に示す。尚、SnO2粉末単独(xが1.0)の場合は、1400℃でも焼結し10なかった。

【0012】 【表1】

【0011】そして、上記各試料につき、平行導体板型*

表 1 [(1-x)TiO2-xSnO2]磁器組成物

No.	×	烧成温皮	Qu	比誘電率	τf	烧粘密度
		(७)	(2. 7~ 7. 1GHz)	ετ	(ppm/C)	(g/cm³)
1 - 1	0	1400	3590	97.1	+ 507	3. 98
1-2	0. 1	1400	3520	84.8	+ 457	4. 22
1-3	0. 2	1400	3280	74.4	+ 423	4. 55
1 - 4	0.3	1400	3440	58.7	+ 343	5.02
1 – 5	0.4	1400	3400	50.2	+ 304	5.35
1 – 6	0.5	1400	3360	42.5	+ 275	5. 55
1 - 7	0.6	1400	3300	34.8	+ 232	5.86
1 – 8	0. 7	1400	3200	27.3	+ 175	6.04
1 – 9	0.8	1400	3490	20.2	+84.3	6. 25
1-10	0. 9	1400	4970	14.0	+ 0.7	6.30
1-11	1. 0	1400	未烧結			
1-12	0	1375	3760	97.7	+ 504	3. 97
1 -13	0.1	1375	3630	84.5	+ 461	4. 21
1-14	0. 2	1375	3 4 0 0	74.6	+ 422	4. 53
1 -15	0.3	1375	3510	59.7	+ 342	5.03
1 -16	0.4	1375	3410	51.6	+ 319	5. 28
1 -17	0. 5	1375	3 4 2 0	43.3	+ 283	5.63
1 -18	0. 6	1 3 7 5	3390	35.0	+ 237	5. 87
1 -19	0. 7	1375	3 2 4 0	27.5	+ 181	6.06
1 -20	0.8	1375	3530	20.5	+ 85	6. 25
1 -21	0.9	1375	5040	14.0	+ 1.2	6.30
1 -22	0. 95	1375	4880	8. 5	-32.4	6.33

[0013]

表 2 [(1-x)TiO₂-xSnO₂]磁器組成物

No.	х	烧成温度	(Qu	比誘電率	τf	烧結密度
		(೪)	(2.6~ 7.1GHz)	ετ	(ppm/℃)	(g/cn°)
2 - 1	0	1350	3670	97.8	+ 506	3. 98
2 – 2	0. 1	1350	3670	84.5	+ 450	4. 21
2 – 3	0. 2	1350	3350	74.6	+ 424	4. 55
2-4	0.3	1350	3350	60.4	+ 343	5.06
2 – 5	0.4	1350	3180	53.1	+ 334	5.33
2 – 6	0. 5	1350	3140	43.9	+ 292	5.62
2 - 7	0.6	1350	3210	34.9	+ 231	5.85
2-8	0.7	1350	3210	27.4	+ 172	6.08
2 – 9	0.8	1350	3380	20.5	+83.4	6. 25
2-10	0.9	1350	4050	14.1	- 1.3	6.30
2-11	0. 9 5	1350	3920	8. 4	-29.2	6.32
2-12	0	1325	3760	97.9	+ 504	3. 97
2-13	0. 1	1 3 2 5	3640	84.0	+ 453	4. 20
2-14	0. 2	1325	3370	74.6	+ 422	4. 55
2-15	0.3	1325	3330	62.3	+ 360	5.06
2-16	0.4	1325	3320	53.7	+ 339	5. 35
2 – 17	0.5	1325	3420	43.4	+ 289	5.63
2-18	0.6	1 3 2 5	3330	34.4	+ 225	5. 88
2-19	0. 7	1325	3190	27.4	+ 160	6. 13
2 -20	0.8	1 3 2 5	3350	20.6	+82.5	6.34
2-21	0. 9	1325	4270	14.3	- 1.6	6.37
2 - 22	0.95	1325	3120	8. 0	-20.0	6.30

[0014]

【表3】

No. x 焼成温度 (で) での 上誘電率 で f (保/cm²) 3-1 0		次 3 [(1-x/)102-x3m02]欧老帝以以7の					
3-1 0 1300 3700 97. 7 + 510 3. 97 3-2 0. 1 1300 3650 83. 8 + 453 4. 19 3-3 0. 2 1300 3370 74. 7 + 430 4. 55 3-4 0. 3 1300 3260 54. 1 + 342 5. 33 3-6 0. 5 1300 3350 43. 2 + 283 5. 62 3-7 0. 6 1300 3350 34. 2 + 220 5. 88 3-8 0. 7 1300 2850 26. 4 + 154 6. 02 3-9 0. 8 1300 3170 20. 1 +83. 7 6. 21 3-10 0. 9 1300 3180 13. 8 − 1. 0 6. 25 3-11 0. 95 1300 1770 6. 5 − 2. 5 6. 10 3-12 0 1275 3770 97. 7 + 505 3. 97 3-13 0. 1 1275 3510 83. 0 + 454 4. 15 3-14 0. 2 1275 3340 75. 1 + 430 4. 55 3-15 0. 3 1275 3200 65. 0 + 385 5. 00 3-16 0. 4 1275 3260 42. 7 + 284 5. 57 3-18 0. 6 1275 3100 33. 5 + 220 5. 80 3-19 0. 7 1275 2580 26. 2 + 153 6. 01 3-20 0. 8 1275 3040 20. 1 +81. 1 6. 19	No.	х	烧成温度		比誘電率	τf	烧結密度
3-2 0. 1 1 3 0 0 3 6 5 0 8 3. 8 + 4 5 3 4. 1 9 3-3 0. 2 1 3 0 0 3 3 7 0 7 4. 7 + 4 3 0 4. 5 5 3-4 0. 3 1 3 0 0 3 3 3 0 6 4. 1 + 3 7 5 5. 0 4 3-5 0. 4 1 3 0 0 3 2 6 0 5 4. 1 + 3 4 2 5. 3 3 3-6 0. 5 1 3 0 0 3 3 5 0 3 4. 2 + 2 8 3 5. 6 2 3-7 0. 6 1 3 0 0 3 3 5 0 3 4. 2 + 2 2 0 5. 8 8 3-8 0. 7 1 3 0 0 2 8 5 0 2 6. 4 + 1 5 4 6. 0 2 3-9 0. 8 1 3 0 0 3 1 7 0 2 0. 1 + 8 3. 7 6. 2 1 3-10 0. 9 1 3 0 0 3 1 8 0 1 3. 8 - 1. 0 6. 2 5 3-11 0. 95 1 3 0 0 1 7 7 0 6. 5 - 2. 5 6. 10 3-12 0 1 2 7 5 3 5 1 0 8 3. 0 + 4 5 4 4. 1 5 3-13 0. 1 1 2 7 5 3 2 0 0 6 5. 0 + 3 8 5 5. 0 0			(७)		ετ	(ppm/℃)	(g/cm ⁸)
3-3 0. 2 1300 3370 74. 7 + 430 4. 55 3-4 0. 3 1300 3330 64. 1 + 375 5. 04 3-5 0. 4 1300 3260 54. 1 + 342 5. 33 3-6 0. 5 1300 3390 43. 2 + 283 5. 62 3-7 0. 6 1300 3350 34. 2 + 220 5. 88 3-8 0. 7 1300 2850 26. 4 + 154 6. 02 3-9 0. 8 1300 3170 20. 1 + 83. 7 6. 21 3-10 0. 9 1300 3180 13. 8 - 1. 0 6. 25 3-11 0. 95 1300 1770 6. 5 - 2. 5 6. 10 3-12 0 1275 3770 97. 7 + 505 3. 97 3-13 0. 1 1275 3340 75. 1 + 430 4. 55 3-15 0. 3 1275 3200 65. 0 + 385 5. 00 3-16 0. 4 1275 3260 <	3-1	0	1300	3700	97. 7	+ 510	3. 97
3-4 0. 3 1300 3330 64. 1 + 375 5. 04 3-5 0. 4 1300 3260 54. 1 + 342 5. 33 3-6 0. 5 1300 3390 43. 2 + 283 5. 62 3-7 0. 6 1300 3350 34. 2 + 220 5. 88 3-8 0. 7 1300 2850 26. 4 + 154 6. 02 3-9 0. 8 1300 3170 20. 1 + 83. 7 6. 21 3-10 0. 9 1300 3180 13. 8 - 1. 0 6. 25 3-11 0. 95 1300 1770 6. 5 - 2. 5 6. 10 3-12 0 1275 3770 97. 7 + 505 3. 97 3-13 0. 1 1275 3510 83. 0 + 454 4. 15 3-14 0. 2 1275 3340 75. 1 + 430 4. 55 3-15 0. 3 1275 3200 65. 0 + 385 5. 00 3-16 0. 4 1275 3260	3 – 2	0.1	1300	3650	83. B	+ 453	4.19
3-5 0. 4 1300 3260 54. 1 + 342 5. 33 3-6 0. 5 1300 3390 43. 2 + 283 5. 62 3-7 0. 6 1300 3350 34. 2 + 220 5. 88 3-8 0. 7 1300 2850 26. 4 + 154 6. 02 3-9 0. 8 1300 3170 20. 1 + 83. 7 6. 21 3-10 0. 9 1300 3180 13. 8 - 1. 0 6. 25 3-11 0. 95 1300 1770 6. 5 - 2. 5 6. 10 3-12 0 1275 3770 97. 7 + 505 3. 97 3-13 0. 1 1275 3510 83. 0 + 454 4. 15 3-14 0. 2 1275 3340 75. 1 + 430 4. 55 3-15 0. 3 1275 3200 65. 0 + 385 5. 00 3-16 0. 4 1275 3260 42. 7 + 284 5. 57 3-18 0. 6 1275 3100	3 – 3	0. 2	1300	3370	74.7	+ 430	4. 55
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	3 – 4	0.3	1300	3330	64.1	+ 375	5.04
3-7 0. 6 1300 3350 34. 2 + 220 5. 88 3-8 0. 7 1300 2850 26. 4 + 154 6. 02 3-9 0. 8 1300 3170 20. 1 +83. 7 6. 21 3-10 0. 9 1300 3180 13. 8 - 1. 0 6. 25 3-11 0. 95 1300 1770 6. 5 - 2. 5 6. 10 3-12 0 1275 3770 97. 7 + 505 3. 97 3-13 0. 1 1275 3510 83. 0 + 454 4. 15 3-14 0. 2 1275 3340 75. 1 + 430 4. 55 3-15 0. 3 1275 3200 65. 0 + 385 5. 00 3-16 0. 4 1275 3320 53. 6 + 341 5. 30 3-17 0. 5 1275 3260 42. 7 + 284 5. 57 3-18 0. 6 1275 3100 33. 5 + 220 5. 80 3-19 0. 7 1275 2580	3 – 5	0.4	1300	3260	54.1	+ 342	5. 33
3-8 0. 7 1 3 0 0 2 8 5 0 2 6. 4 + 1 5 4 6. 0 2 3-9 0. 8 1 3 0 0 3 1 7 0 2 0. 1 + 8 3. 7 6. 2 1 3-10 0. 9 1 3 0 0 3 1 8 0 1 3. 8 - 1. 0 6. 2 5 3-11 0. 95 1 3 0 0 1 7 7 0 6. 5 - 2. 5 6. 1 0 3-12 0 1 2 7 5 3 7 7 0 9 7. 7 + 5 0 5 3. 9 7 3-13 0. 1 1 2 7 5 3 5 1 0 8 3. 0 + 4 5 4 4. 1 5 3-14 0. 2 1 2 7 5 3 3 4 0 7 5. 1 + 4 3 0 4. 5 5 3-15 0. 3 1 2 7 5 3 2 0 0 6 5. 0 + 3 8 5 5. 0 0 3-16 0. 4 1 2 7 5 3 2 6 0 4 2. 7 + 2 8 4 5. 5 7 3-18 0. 6 1 2 7 5 3 1 0 0 3 3. 5 + 2 2 0 5. 8 0 3-19 0. 7 1 2 7 5 2 5 8 0 2 6. 2 + 1 5 3 6. 0 1 3-20 0. 8 1 2 7 5 3 0 4 0 2 0. 1 + 8 1. 1 6. 1 9	3-6	0.5	1300	3390	43. 2	+ 283	5. 62
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	3-7	0.6	1300	3350	34. 2	+ 220	5.88
3-10 0.9 1300 3180 13.8 - 1.0 6.25 3-11 0.95 1300 1770 6.5 - 2.5 6.10 3-12 0 1275 3770 97.7 + 505 3.97 3-13 0.1 1275 3510 83.0 + 454 4.15 3-14 0.2 1275 3340 75.1 + 430 4.55 3-15 0.3 1275 3200 65.0 + 385 5.00 3-16 0.4 1275 3320 53.6 + 341 5.30 3-17 0.5 1275 3260 42.7 + 284 5.57 3-18 0.6 1275 3100 33.5 + 220 5.80 3-19 0.7 1275 2580 26.2 + 153 6.01 3-20 0.8 1275 3040 20.1 +81.1 6.19	3-8	0. 7	1300	2850	26.4	+ 154	6.02
3-11 0. 95 1 3 0 0 1 7 7 0 6. 5 - 2. 5 6. 1 0 3-12 0 1 2 7 5 3 7 7 0 9 7. 7 + 5 0 5 3. 9 7 3-13 0. 1 1 2 7 5 3 5 1 0 8 3. 0 + 4 5 4 4. 1 5 3-14 0. 2 1 2 7 5 3 3 4 0 7 5. 1 + 4 3 0 4. 5 5 3-15 0. 3 1 2 7 5 3 2 0 0 6 5. 0 + 3 8 5 5. 0 0 3-16 0. 4 1 2 7 5 3 2 6 0 4 2. 7 + 2 8 4 5. 5 7 3-18 0. 6 1 2 7 5 3 1 0 0 3 3. 5 + 2 2 0 5. 8 0 3-19 0. 7 1 2 7 5 2 5 8 0 2 6. 2 + 1 5 3 6. 0 1 3-20 0. 8 1 2 7 5 3 0 4 0 2 0. 1 + 8 1. 1 6. 1 9	3 — 9	0.8	1300	3170	20.1	+83.7	6. 21
3-12 0 1 2 7 5 3 7 7 0 9 7. 7 + 5 0 5 3. 9 7 3-13 0. 1 1 2 7 5 3 5 1 0 8 3. 0 + 4 5 4 4. 1 5 3-14 0. 2 1 2 7 5 3 3 4 0 7 5. 1 + 4 3 0 4. 5 5 3-15 0. 3 1 2 7 5 3 2 0 0 6 5. 0 + 3 8 5 5. 0 0 3-16 0. 4 1 2 7 5 3 3 2 0 5 3. 6 + 3 4 1 5. 3 0 3-17 0. 5 1 2 7 5 3 2 6 0 4 2. 7 + 2 8 4 5. 5 7 3-18 0. 6 1 2 7 5 3 1 0 0 3 3. 5 + 2 2 0 5. 8 0 3-19 0. 7 1 2 7 5 2 5 8 0 2 6. 2 + 1 5 3 6. 0 1 3-20 0. 8 1 2 7 5 3 0 4 0 2 0. 1 + 8 1. 1 6. 1 9	3-10	0. 9	1300	3180	13.8	- 1.0	6. 25
3-13 0. 1 1 2 7 5 3 5 1 0 8 3. 0 + 4 5 4 4. 1 5 3-14 0. 2 1 2 7 5 3 3 4 0 7 5. 1 + 4 3 0 4. 5 5 3-15 0. 3 1 2 7 5 3 2 0 0 6 5. 0 + 3 8 5 5. 0 0 3-16 0. 4 1 2 7 5 3 3 2 0 5 3. 6 + 3 4 1 5. 3 0 3-17 0. 5 1 2 7 5 3 2 6 0 4 2. 7 + 2 8 4 5. 5 7 3-18 0. 6 1 2 7 5 3 1 0 0 3 3. 5 + 2 2 0 5. 8 0 3-19 0. 7 1 2 7 5 2 5 8 0 2 6. 2 + 1 5 3 6. 0 1 3-20 0. 8 1 2 7 5 3 0 4 0 2 0. 1 + 8 1. 1 6. 1 9	3-11	0.95	1300	1770	6. 5	- 2.5	6. 10
3-14 0. 2 1 2 7 5 3 3 4 0 7 5. 1 + 4 3 0 4. 5 5 3-15 0. 3 1 2 7 5 3 2 0 0 6 5. 0 + 3 8 5 5. 0 0 3-16 0. 4 1 2 7 5 3 3 2 0 5 3. 6 + 3 4 1 5. 3 0 3-17 0. 5 1 2 7 5 3 2 6 0 4 2. 7 + 2 8 4 5. 5 7 3-18 0. 6 1 2 7 5 3 1 0 0 3 3. 5 + 2 2 0 5. 8 0 3-19 0. 7 1 2 7 5 2 5 8 0 2 6. 2 + 1 5 3 6. 0 1 3-20 0. 8 1 2 7 5 3 0 4 0 2 0. 1 + 8 1. 1 6. 1 9	3-12	0	1 2 7 5	3770	97.7	+ 505	3. 97
3-15 0. 3 1 2 7 5 3 2 0 0 6 5. 0 + 3 8 5 5. 0 0 3-16 0. 4 1 2 7 5 3 3 2 0 5 3. 6 + 3 4 1 5. 3 0 3-17 0. 5 1 2 7 5 3 2 6 0 4 2. 7 + 2 8 4 5. 5 7 3-18 0. 6 1 2 7 5 3 1 0 0 3 3. 5 + 2 2 0 5. 8 0 3-19 0. 7 1 2 7 5 2 5 8 0 2 6. 2 + 1 5 3 6. 0 1 3-20 0. 8 1 2 7 5 3 0 4 0 2 0. 1 + 8 1. 1 6. 1 9	3-13	0.1	1275	3510	83.0	+ 454	4. 15
3-16 0. 4 1 2 7 5 3 3 2 0 5 3. 6 + 3 4 1 5. 3 0 3-17 0. 5 1 2 7 5 3 2 6 0 4 2. 7 + 2 8 4 5. 5 7 3-18 0. 6 1 2 7 5 3 1 0 0 3 3. 5 + 2 2 0 5. 8 0 3-19 0. 7 1 2 7 5 2 5 8 0 2 6. 2 + 1 5 3 6. 0 1 3-20 0. 8 1 2 7 5 3 0 4 0 2 0. 1 + 8 1. 1 6. 1 9	3 – 14	0. 2	1275	3 3 4 0	75.1	+ 430	4. 55
3-17 0. 5 1 2 7 5 3 2 6 0 4 2. 7 + 2 8 4 5. 5 7 3-18 0. 6 1 2 7 5 3 1 0 0 3 3. 5 + 2 2 0 5. 8 0 3-19 0. 7 1 2 7 5 2 5 8 0 2 6. 2 + 1 5 3 6. 0 1 3-20 0. 8 1 2 7 5 3 0 4 0 2 0. 1 + 8 1. 1 6. 1 9	3 – 15	0.3	1275	3200	65.0	+ 385	5.00
3-18 0. 6 1 2 7 5 3 1 0 0 3 3. 5 + 2 2 0 5. 8 0 3-19 0. 7 1 2 7 5 2 5 8 0 2 6. 2 + 1 5 3 6. 0 1 3-20 0. 8 1 2 7 5 3 0 4 0 2 0. 1 + 8 1. 1 6. 1 9	3-16	0.4	1275	3320	53.6	+ 341	5.30
3-19 0. 7 1 2 7 5 2 5 8 0 2 6. 2 + 1 5 3 6. 0 1 3-20 0. 8 1 2 7 5 3 0 4 0 2 0. 1 + 8 1. 1 6. 1 9	3 – 17	0.5	1275	3260	42.7	+ 284	5. 57
3-20 0. 8 1275 3040 20. 1 +81. 1 6. 19	3-18	0.6	1275	3100	33.5	+ 220	5.80
	3 19	0. 7	1 2 7 5	2580	26.2	+ 153	6. D 1
3-21 0. 9 1275 3120 13. 6 + 0. 1 6. 18	3 - 20	0.8	1 2 7 5	3040	20.1	+81.1	6. 19
	3 -21	0. 9	1275	3120	13.6	+ 0.1	6. 18
3-22 0.95 1275 未烧結 5.94	3 – 22	0.95	1275				5. 94

【0015】これらの結果によれば、xが0.9では、 Quが飛躍的に増大し(図1及び表1のNo. 1-2 1、表2のNo. 2-21) した。また、 τ f は表1~ 3に示すxが0.9のいずれの場合も飛躍的に減少し て、-1.6~+1.2ppm/℃となり、0近辺の極 めて優れた性能を示した。特に、焼成温度が1375℃ 及び1325℃の場合は、各々、Quが5040、42 70、εr \hbar 14.0、14.3、 τ f \hbar +1.2pp m/\mathbb{C} 、-1. 6 p p m/\mathbb{C} となり、 ε r が小さ目であ るものの、全体して大変優れたバランス性能を示した。 【0016】xが0.8~0.9の場合は、Quが14 10~5040 (xが0.9のNo.3-10及びxが 40 ラフである。 0.9のNo.3-22を除くと、3040~504 0)、εrが13.6~20.6及びτ,が-1.6~ +85ppm/℃となり、バランスのとれた性能を示 す。また、 τ fを0近辺の値に自由に調整できる。尚、 本発明においては、前記具体的実施例に示すものに限ら れず、目的、用途に応じて本発明の範囲内で種々変更し た実施例とすることができる。

[0017]

【発明の効果】本第1発明の誘電体磁器組成物は、Q u、 ϵ ,及び τ ,をいずれも実用的な特性範囲に維持し つつ、高い焼結密度を示し、更に単純組成である。ま た、本第2発明の製造方法によれば、広い温度範囲内に おいて焼成温度を種々変動させても、上記有用な誘電体 磁器組成物を安定して製造できるとともに、 τ fを0近 辺に自由に調整できる。

【図面の簡単な説明】

【図1】焼成温度1375℃における(1-x) TiO 2-xSnO2磁器組成物のxとQuとの関係を示すグ

【図2】図1にて示す磁器組成物において、 $x \geq \epsilon_r$ と の関係を示すグラフである。

【図3】図1にて示す磁器組成物において、 $x と \tau$, と の関係を示すグラフである。

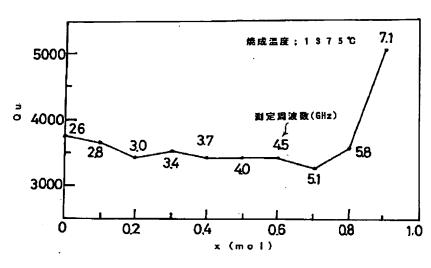
【図4】図1にて示す磁器組成物において、xと焼結密 度との関係を示すグラフである。

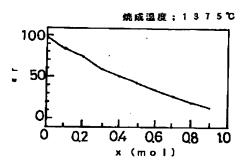


【図2】



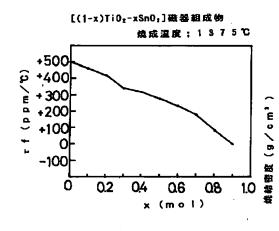
[(1-x)TiO,-xSnO,]磁器組成物

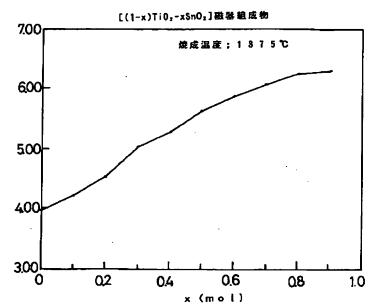




【図3】

【図4】





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CLAIMS

[Claim(s)]

[Claim 1] Empirical formula (1-x) TiO2-xSnO2 A dielectric-ceramics-for-microwave porcelain constituent characterized by consisting of a presentation expressed with [0.8<=x<1.0 [however,]]. [Claim 2] Empirical formula (1-x) TiO2-xSnO2 A manufacture method of a dielectric-ceramics-for-microwave porcelain constituent which mixes titanium oxide (IV) powder and tin oxide (IV) powder so that it may become the presentation shown by [0.8<=x<1.0 [however,]], carries out temporary quenching after that, manufactures temporary-quenching powder, grinds this temporary-quenching powder, fabricates in a predetermined configuration, and is subsequently characterized by calcinating at 1275-1400 degrees C.

[Translation done.]

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DETAILED DESCRIPTION

[Detailed Description of the Invention] [0001]

[Industrial Application] This invention relates to the dielectric-ceramics-for-microwave porcelain constituent in which high sintered density is shown, maintaining each temperature coefficient (only henceforth tauf) of unloaded Q (only henceforth Qu), specific inductive capacity (only henceforth epsilonr), and resonance frequency in the practical property range, if it says in more detail about a dielectric-ceramics-for-microwave porcelain constituent. This invention is used for the impedance matching of a dielectric resonator, the microwave accumulation circuit board, and various microwave circuits etc. in a microwave range.

[10002]

[Description of the Prior Art] It has high unloaded Q and a high dielectric constant in the dielectric resonator and dielectric substrate which are generally used for RF fields, such as microwave and a millimeter wave, and, moreover, they are expected what has the small absolute value of resonance frequency. That is, since a dielectric-ceramics-for-microwave porcelain constituent (only henceforth a dielectric porcelain constituent) is in the inclination for dielectric loss to become large as operating frequency serves as a RF, a big dielectric porcelain constituent of Qu is desired in the microwave range. Moreover, as an empirical formula (1-x) TiO2-xSnO2 system dielectric porcelain material, the thing of 0.5 is known for x ("ceramic engineering handbook" (issuance: Ceramic Society of Japan, P.1885).). [0003]

[Problem(s) to be Solved by the Invention] However, above-mentioned TiO2-SnO2 With a system dielectric porcelain material, Q (7GHz) is 4500 and epsilonr. Although it was as large as 43, tauf was dramatically as large as +250ppm/degree C, and there was a problem that it was difficult to adjust to the small value of the zero neighborhood.

[0004] This invention solves the above-mentioned trouble and is Qu and epsilonr. And tauf It aims at offering the dielectric porcelain constituent and its manufacture method of the simple presentation which shows high sintered density, maintaining each in a practical property range.

[0005]

[Means for Solving the Problem] this invention persons set to a dielectric porcelain constituent of a simple presentation, and are Qu and epsilonr. And tauf Maintaining each in a practical property range As a result of examining many things about a presentation which shows high sintered density, it is TiO2-SnO2. By making it a predetermined presentation rate in a system, Qu becomes large by leaps and bounds, and tauf finds out a presentation range which can be adjusted in the 0 neighborhood, and it came to complete this invention. That is, a dielectric porcelain constituent of **** 1 invention is empirical formula (1-x) TiO2-xSnO2. It is characterized by consisting of a presentation expressed with [0.8<=x<1.0 [however,]].

[0006] A manufacture method of a dielectric porcelain constituent **** 2 invention is empirical formula (1-x) TiO2-xSnO2. Titanium oxide (IV) powder and tin oxide (IV) powder are mixed so that it may become the presentation shown by [0.8<=x<1.0 [however,]], temporary quenching and grinding are

performed after that, and it fabricates in a predetermined configuration, and, subsequently is characterized by calcinating at 1275-1400 degrees C.

[0007] Empirical formula (1-x) TiO2-xSnO2 When x is less than 0.8, it is tauf which set and made the range of x less than [0.8 or more] into 1.0. A positive big value is taken and Qu is from a small value being shown relatively (that is, it becoming a big value by leaps and bounds, when x is 0.9.). Conversely, it is because it already winds and eburnation is not carried out in 1400 degrees C, when this is 1.0. Burning temperature was made into the range of 1275-1400 degrees C because a property would deteriorate gradually at a temperature lower than 1275 degrees C, if eburnation may not be carried out well and 1400 degrees C was exceeded conversely.

[0008] According to the experimental result especially shown in a table 1, by case (x is 0.9) where burning temperature is 1375 degrees C and 1325 degrees C, Qu increased by leaps and bounds. For example, x is 0.9, and burning temperature becomes 5040 (7.1GHz), epsilonr =14.0, and tauf =+1.2ppm/degree C at 1375 degrees C, and Qu is epsilonr. Although it is a little small, Qu shows maximum, and it is tauf. It becomes the zero neighborhood and extremely excellent balance engine performance is shown. Furthermore, even if it calcinates in a large temperature requirement of 1275-1400 degrees C about burning temperature, engine performance which was excellent while there was comparatively little variation in each engine performance is shown.

[Example] Hereafter, an example explains this invention concretely. TiO2 Powder (purity; 99.95%) and SnO2 powder (purity; 99.3%) -- a start raw material -- carrying out -- empirical formula (1-x) TiO2-xSnO2 it becomes the presentation from which x changed -- as -- the specified quantity (about 500g as the whole quantity) -- weighing capacity -- it mixed. Then, after giving mixing (20 - 30 minutes) and primary grinding by dry type by the mixer, temporary quenching was carried out at the temperature of 1050 degrees C in the atmospheric-air ambient atmosphere for 2 hours. Subsequently, the organic binder (29g) and water (400-450g) of optimum dose were added to this temporary-quenching powder, and the alumina balls of 20mmphi ground 90 rpm for 23 hours. Then, it corns by freeze-drying (about 0.4 degree of vacuum Torr(s), freezing-point-20--40 degree C, drying temperature of 40-50 degrees C, vacuum-drying time amount about 20 hours), this raw material by which the granulation was carried out is used, and it is 2 1t/cm. It fabricated by press ** in the shape of [of 19mmphix11mmt (height)] a cylinder.

[0010] This Plastic solid is degreased among atmospheric air in 500 degrees C and 3 hours. Next, at each temperature of the range of 1275-1400 degrees C after that It calcinated for 4 hours, finally the ends side was ground in the shape of [of abbreviation 16mmphix8mmt (height)] a cylinder, and it considered as the dielectric sample (No.1-1-1-22, 2-1 to 2-22, and 3-1 to 3-22 of tables 1-3). In addition, 100 degrees C [h] /and the temperature fall speed of the programming rate [in / in a programming rate / in / programming rate / in the above-mentioned temporary-quenching process / in 200 degrees C / h / /and temperature fall speed / -200 degrees C / h / /and this degreasing process / 50 degrees C / h / /and a baking process] were -100 degrees C/h.

[0011] and each above-mentioned sample -- attaching -- parallel -- a conductor -- a stencil dielectric cylinder resonator method (TE011 MODE) -- Qu and epsilonr And tauf was measured. Sintered density was measured by the Archimedes method. In addition, resonance frequency is 2.6-7.1GHz. Moreover, tauf It measured in the 23-80-degree C temperature field, and computed at tauf =(f80-f23)/(f23xdeltaT) and deltaT=80 degree-C-23 degree-C=57 degree C. These results are shown in tables 1-3 (burning temperature; 1275-1400 degrees C) and drawing 1 -4 (burning temperature; 1375 degrees C). In addition, SnO2 When it was powder independent (x is 1.0), at least 1400 degrees C were not sintered. [0012]

[A table 1]

表1 [(1-x)TiO2-xSnO2]磁器組成物

No.	x	焼成温皮	Qu	比誘電率	rf	烧結密度
		(७)	(2. 7~ 7. 1Gliz)	εΓ	(ppm∕C)	(g/cm³)
1-1	0	1400	3590	97.1	+ 507	3. 98
1-2	0. 1	1400	3520	84.8	+ 457	4. 22
1-3	0. 2	1400	3280	74.4	+ 423	4. 55
1 – 4	0.3	1400	3440	58.7	+ 343	5.02
1 – 5	0.4	1400	3400	50.2	+ 304	5.35
1 – 6	0.5	1400	3360	42.5	+ 275	5. 55
1 – 7	0.6	1400	3300	34.8	+ 232	5.86
1 – 8	0.7	1400	3200	27.3	+ 175	6.04
1 – 9	0.8	1400	3490	20.2	+84.3	6. 25
1-10	0. 9	1400	4970	14.0	+ 0.7	6.30
1-11	1. 0	1400		未	差結	
1-12	0	1375	3760	97.7	+ 504	3. 97
1 -13	0.1	1375	3630	84.5	+ 461	4. 21
1-14	0. 2	1375	3400	74.6	+ 422	4. 53
1 -15	0.3	1375	3510	59.7	+ 342	5.03
1 -16	0.4	1375	3410	51.6	+ 319	5. 28
1-17	0.5	1375	3 4 2 0	43.3	+ 283	5. 63
1 -18	0.6	1375	3 3 9 0	35.0	+ 237	5. 87
1-19	0. 7	1 3 7 5	3 2 4 0	27.5	+ 181	6.06
1 -20	0.8	1375	3530	20.5	+ 85	6. 25
1 -21	0.9	1375	5040	14.0	+ 1.2	6.30
1 -22	0.95	1375	4880	8. 5	-32.4	6.33

[0013] [A table 2]

表2 [(1-x)TiO₂-xSnO₂]磁器組成物

No.	х	烧成温度	Q u (2.6~	比誘電率	τf	烧結密度
		(७)	7. 1GHz)	εr	(pp@/℃)	(g/cm³)
2-1	0	1350	3670	97.8	+ 506	3. 98
2 – 2	0. 1	1350	3670	84.5	+ 450	4. 21
2 - 3	0. 2	1350	3350	74.6	+ 424	4. 55
2-4	0. 3	1350	3 3 5 0	60.4	+ 343	5.06
2 – 5	0.4	1350	3180	53.1	+ 334	5. 33
2-6	0.5	1350	3140	43.9	+ 292	5.62
2-7	0.6	1350	3210	34.9	+ 231	5.85
2-8	0.7	1350	3210	27.4	+ 172	6.08
2 – 9	0.8	1350	3380	20.5	+83.4	6. 25
2-10	0.9	1350	4050	14.1	- 1.3	6.30
2-11	0.95	1350	3920	8. 4	-29.2	6.32
2-12	0	1325	3760	97.9	+ 504	3. 97
2-13	0.1	1325	3640	84.0	+ 453	4.20
2-14	0. 2	1325	3370	74.6	+ 422	4.55
2-15	0.3	1325	3 3 3 0	62.3	+ 360	5.06
2-16	0.4	1325	3320	53.7	+ 339	5. 35
2-17	0.5	1 3 2 5	3 4 2 0	43.4	+ 289	5.63
2-18	0.6	1 3 2 5	3330	34.4	+ 225	5.88
2-19	0. 7	1325	3190	27. 4	+ 160	6. 13
2 -20	0.8	1325	3 3 5 0	20.6	+82.5	6.34
2 -21	0.9	1325	4270	14.3	- 1.6	6.37
2 - 22	0.95	1325	3120	8. 0	-20.0	6.30

[0014] [A table 3]

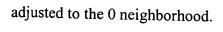
表3 [(1-x)TiO2-xSnO2]磁器組成物

No. 3 - 1	х	烧成温度	E Qu	11.05.55	· T	
3-1	1		(2.6~	比誘電準	T f	烧結密度
3-1		(3)	7. 0GHz)	εr	(ppm/で)	(g/cm³)
		1300	3700	97.7	+ 510	3. 97
3-2	0.1	1300	3650	83.8	 	
3 - 3	0. 2	1300	3370	74. 7	+ 430	
3 - 4	0. 3	1300	3330	64.1	+ 375	
3 - 5	0.4	1300	3260	54.1	+ 342	
3 - 6	0. 5	1300	3390	43. 2	+ 283	
3 - 7	0.6	1300	3350	34. 2	+ 220	5. 88
3 - 8	0. 7	1300	2850	26.4	+ 154	6. 02
3 – 9	0.8	1300	3170	20.1	+83.7	6. 21
3 - 10	0. 9	1300	3180	13.8	- 1.0	6. 25
3 - 11	0.95	1300	1770	6. 5	- 2.5	6. 10
3-12	0	1275	3770	9 7. 7	+ 505	3. 97
3-13	0.1	1275	3510	83.0	+ 454	4. 15
3-14	0. 2	1275	3 3 4 0	75.1	+ 430	4. 55
3-15	0.3	1275	3200	65.0	+ 385	5. 00
3-16	0.4	1 2 7 5	3 3 2 0	53.6	+ 341	5. 30
3-17	0.5	1275	3260	42. 7	+ 284	5. 57
3-18	0.6	1275	3100	33.5	+ 220	5. 80
3-19	0. 7	1275	2580	26. 2	+ 153	6. 01
3-20	0.8	1275	3040	20.1	+81.1	6. 19
3-21	0. 9	1275	3120	100	+ 0. 1	6. 18
3-22	0.95	1275		未烧結		5. 94

[0015] According to these results, by 0.9, Qu increased by leaps and bounds and x carried out (No.1-21 of drawing 1 and a table 1, No.2-21 of a table 2). Moreover, tauf decreased by leaps and bounds, also when x shown in tables 1-3 was any of 0.9, it became in degree C and -1.6-+1.2 ppm /, and showed the engine performance which was extremely excellent in the 0 neighborhood. Especially when burning temperature was 1375 degrees C and 1325 degrees C, Qu showed respectively the balance engine performance which 14.0, 14.3, and tauf became [5040, 4270, and epsilonr] in +1.2ppm/degree C and degree C and -1.6 ppm /, carried out the whole although epsilonr was eye small **, and was very

[0016] When x is 0.8-0.9, for Qu, 1410-5040 (x No.3- of 0.9 10 and x No. of 0.9 3 if -22 is removed 3040-5040), and epsilonr are 13.6-20.6, and tauf. It becomes in degree C and -1.6-+85 ppm /, and the neighborhood. In addition, in this invention, it is not restricted to what is shown in said concrete example, but can consider as the example variously changed within the limits of this invention [0017]

[Effect of the Invention] The dielectric porcelain constituent of **** 1 invention is Qu and epsilonr. And tauf Maintaining each in a practical property range, high sintered density is shown and it is a simple presentation further. moreover -- even if it fluctuates various burning temperature in a large temperature requirement according to the manufacture method of **** 2 invention -- the above -- while being stabilized and being able to manufacture a useful dielectric porcelain constituent, tauf can be freely



[Translation done.]